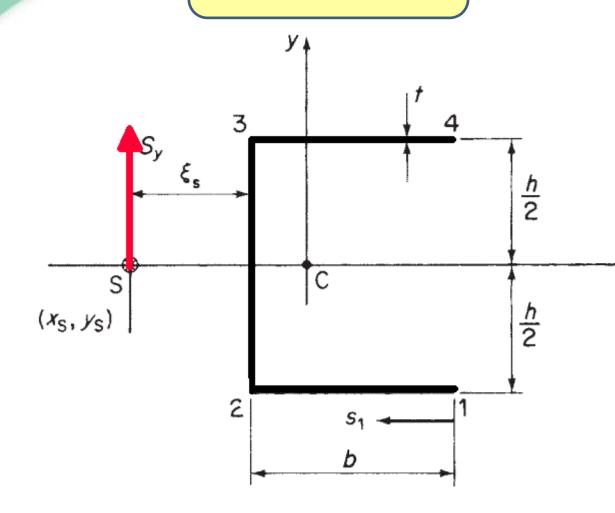
### **Shear Center of open thin-walled beams**



#### **EQUIVALENCE** of:

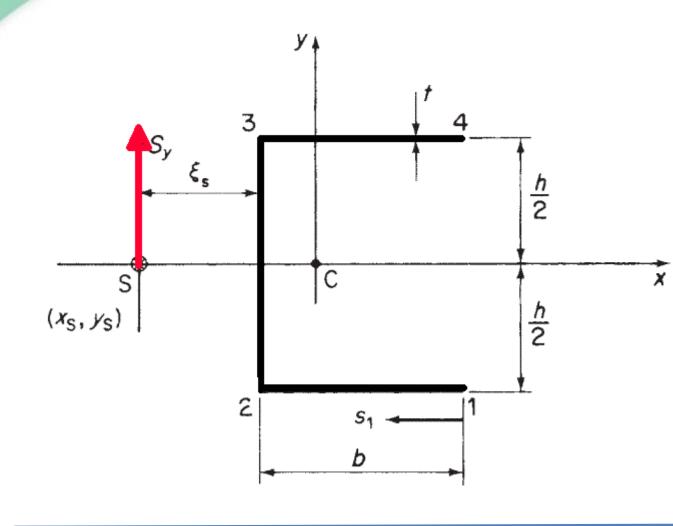
**Cause** (external load,  $S_x$  and  $S_y$ )

and

**Result** (created shear stress)

Logical choice – <u>equivalence of moment</u> w.r.t. arbitrary chosen location

#### **Shear Center of open thin-walled beams**



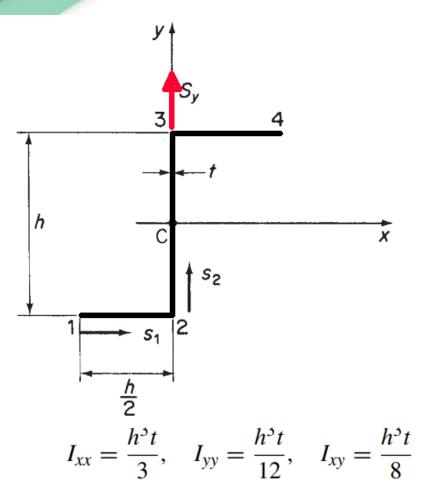
$$q_{s} = -\frac{S_{y}}{I_{xx}} \int_{0}^{s} ty \, ds$$

$$I_{xx} = 2bt \left(\frac{h}{2}\right)^{2} + \frac{th^{3}}{12} = \frac{h^{3}t}{12} \left(1 + \frac{6b}{h}\right)$$

$$q_{s} = \frac{-12S_{y}}{h^{3}(1 + 6b/h)} \int_{0}^{s} y \, ds$$

$$q_{12} = \frac{6S_{y}}{h^{2}(1 + 6b/h)} s_{1}$$

$$\xi_{s} = \frac{3b^{2}}{h(1 + 6b/h)}$$



$$q_{s} = \frac{S_{y}}{h^{3}} \int_{0}^{s} (10.32x - 6.84y) ds$$
  
On the bottom flange 12,  $y = -h/2$  and  $x = -h/2 + s_{1}$ , where  $0 \le s_{1} \le h/2$ .  
$$q_{12} = \frac{S_{y}}{h^{3}} \int_{0}^{s_{1}} (10.32s_{1} - 1.74h) ds_{1}$$

$$q_{12} = \frac{S_y}{h^3} (5.16s_1^2 - 1.74hs_1)$$

Hence at 1 (s1 = 0),  $q_1 = 0$ and at 2 (s1 = h/2),  $q_2 = 0.42S_y/h$ .

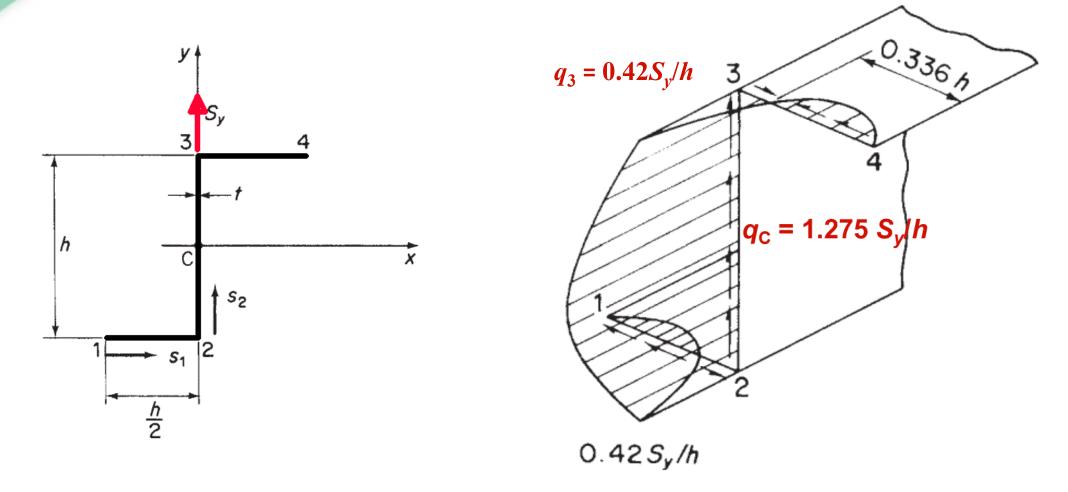
y h X S2 S1  $\frac{h}{2}$   $I_{xx} = \frac{h^3 t}{3}, \quad I_{yy} = \frac{h^3 t}{12}, \quad I_{xy} = \frac{h^3 t}{8}$ 

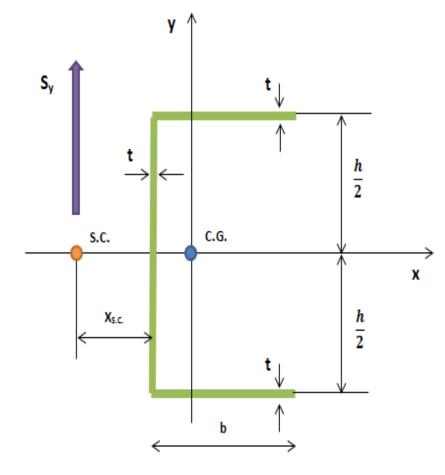
In the web 23,  $y = -h/2 + s_2$ , where  $0 \le s_2 \le h$  and x = 0. Then

$$q_{23} = \frac{S_y}{h^3} \int_0^{s_2} (3.42h - 6.84s_2) \mathrm{d}s_2 + q_2$$

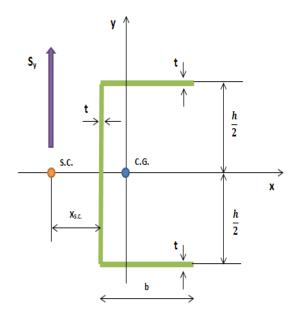
$$q_{23} = \frac{S_y}{h^3}(0.42h^2 + 3.42hs_2 - 3.42s_2^2)$$

At C point  $(s_2 = h/2)$  there is maximum, and  $q_C = 1.275 S_y/h$ .



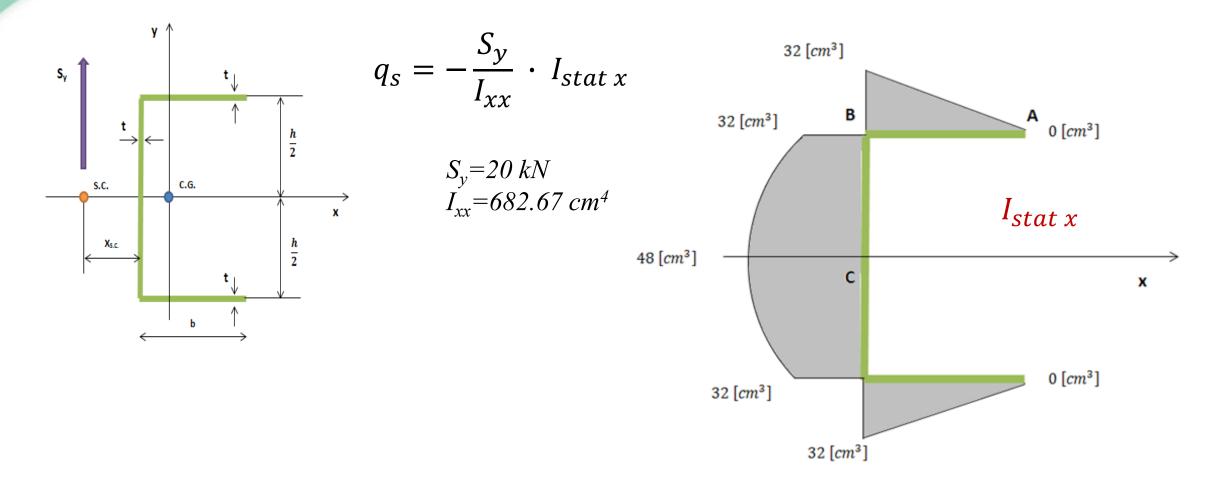


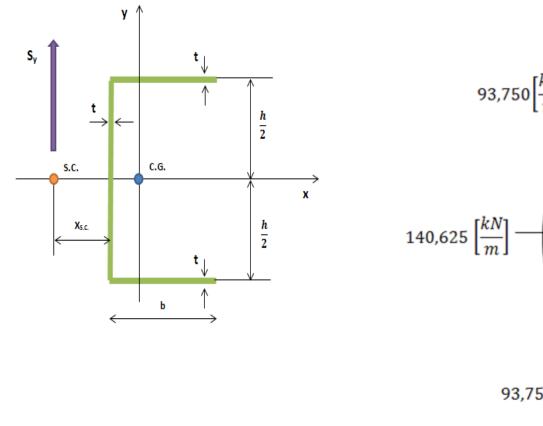
S.C. – shear center C.G. – center of gravity

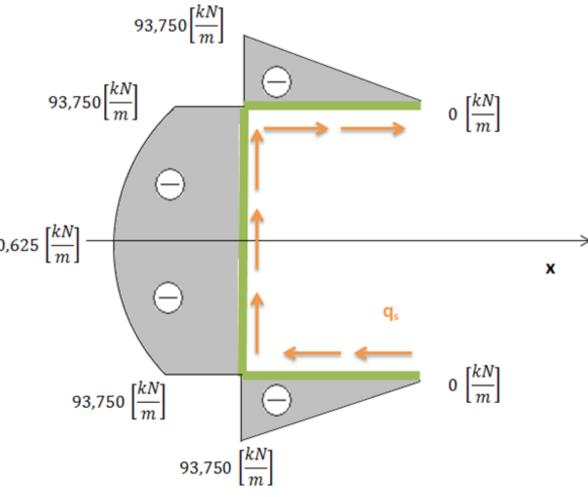


$$I_{xx} = \frac{t \cdot h^3}{12} + 2 \cdot \left[\frac{b \cdot t^3}{12} + t \cdot b \cdot \left(\frac{h}{2}\right)^2\right]$$
$$= \frac{0.5 \cdot 16^3}{12} + 2 \cdot \left[0 + 0.5 \cdot 8 \cdot \left(\frac{16}{2}\right)^2\right]$$
where the following assumption can be written:
$$\frac{b \cdot t^3}{12} \approx 0$$
thus

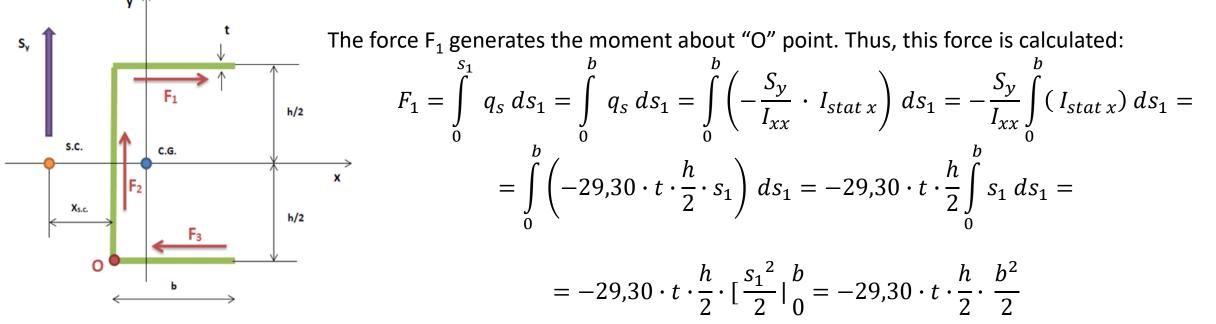
 $I_{xx} = 170,66 + 512 = 682,67 \ [cm^4] = 682,67 \ \cdot 10^4 \ [mm^4]$ 





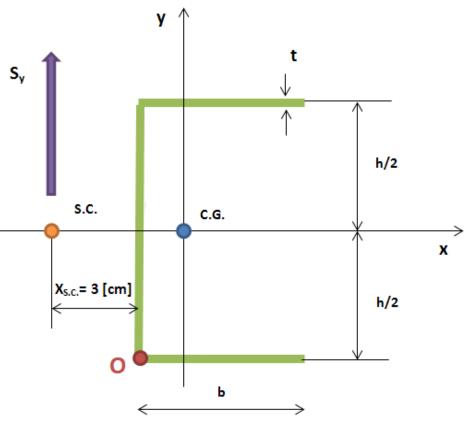


$$S_y \cdot x_{S.C.} = F_1 \cdot h$$



The range is  $s_1 \in \langle 0 \rangle$ ; b >where b = 8[cm], thus:

$$F_1 = -29,30 \frac{[N]}{[cm^4]} \cdot 0,5 \ [cm] \cdot \frac{16}{2} \ [cm] \cdot \frac{(8 \ [cm])^2}{2} = -29,30 \cdot 0,5 \cdot 4 \cdot 32 \ [N] = -3750 \ [N]$$



Calculation of the coordinate of the shear center

$$x_{S.C.} = \frac{F_1 \cdot h}{S_y} = \frac{-3750 \ [N] \cdot 0,16 \ [m]}{2 \cdot 10^4 \ [N]} = -0,03 \ [m] = -3 \ [cm]$$

The minus sign means that the shear center position lies opposite to the "X" axis, so to the left from the "O" point.

# **Thin-walled beams – bending / shear**

**NOW** generalized for closed section

## **Recall - Shear of open thin-walled beams**

 $\frac{\partial q}{\partial s} + t \frac{\partial \sigma_z}{\partial z} = 0 \qquad \qquad \frac{\partial \sigma_z}{\partial z} = \frac{\left[(\partial M_y/\partial z)I_{xx} - (\partial M_x/\partial z)I_{xy}\right]}{I_{xx}I_{yy} - I_{xy}^2} x + \frac{\left[(\partial M_x/\partial z)I_{yy} - (\partial M_y/\partial z)I_{xy}\right]}{I_{xx}I_{yy} - I_{xy}^2} y$ 

$$\frac{\partial q}{\partial s} = -\frac{(S_x I_{xx} - S_y I_{xy})}{I_{xx} I_{yy} - I_{xy}^2} tx - \frac{(S_y I_{yy} - S_x I_{xy})}{I_{xx} I_{yy} - I_{xy}^2} ty$$

$$q_{s} = -\left(\frac{S_{x}I_{xx} - S_{y}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} tx \, ds - \left(\frac{S_{y}I_{yy} - S_{x}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} ty \, ds$$

$$q_s = -\frac{S_x}{I_{yy}} \int_0^s tx \, \mathrm{d}s - \frac{S_y}{I_{xx}} \int_0^s ty \, \mathrm{d}s$$

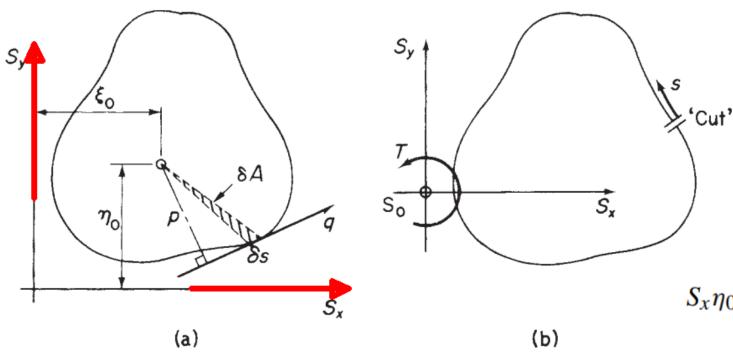
### Shear of closed section thin-walled beams

$$q_{s} = -\left(\frac{S_{x}I_{xx} - S_{y}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} tx \, ds - \left(\frac{S_{y}I_{yy} - S_{x}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} ty \, ds$$
$$q_{s} - q_{s,0} = -\left(\frac{S_{x}I_{xx} - S_{y}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} tx \, ds - \left(\frac{S_{y}I_{yy} - S_{x}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} ty \, ds$$

$$q_s = q_{\rm b} + q_{s,0}$$

$$q_{s} = -\left(\frac{S_{x}I_{xx} - S_{y}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} tx \, ds - \left(\frac{S_{y}I_{yy} - S_{x}I_{xy}}{I_{xx}I_{yy} - I_{xy}^{2}}\right) \int_{0}^{s} ty \, ds + q_{s,0}$$

#### Shear of closed section thin-walled beams



**EQUIVALENCE** of:

**Cause** (external load,  $S_x$  and  $S_y$ )

and

**Result** (created shear stress)

$$S_x \eta_0 - S_y \xi_0 = \oint pq \, \mathrm{d}s = \oint pq_b \, \mathrm{d}s + q_{s,0} \oint p \, \mathrm{d}s$$

$$S_x \eta_0 - S_y \xi_0 = \oint p q_{\rm b} \mathrm{d}s + \frac{2Aq_{s,0}}{2}$$

# **Shear Center of closed section thin-walled beams**

It is necessary to use the ADDITIONAL information: condition that a shear load acting through the shear centre of a section produces zero twist.

$$\frac{\mathrm{d}\theta}{\mathrm{d}z} = \frac{1}{2A} \oint \frac{q_s}{Gt} \mathrm{d}s$$

## **Shear Center of closed section thin-walled beams**

